# **1D Coaxial Photonic Crystal - Superluminal**

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J. N. Munday and W. M. Robertson have reported observing: *Negative group velocity pulse tunneling through a coaxial photonic crystal*, Applied Physics Letters, Sept. 2002. In the following, we analyze this situation using Mathcad.

When a signal traverses an impedance boundary, it experiences a phase shift and a partial reflection that can be calculated from the generalized optical Fresnel coefficients of reflection r (IVreflected/VincidentI) and transmission t IVtransmitted/VincidentI). This can be generalized to coaxial cables using characteristic impedance, where zi, zr and zt are the impedance of the incident, refelected and transmitted media.  $r = \frac{zi - zt}{t} = \frac{2 \cdot zi}{t}$ 

$$=\frac{z_1-z_1}{z_1+z_1} \qquad t=\frac{z_1z_1}{z_1+z_1}$$

Periodic variation in the impedance of a medium can produce destructive interference for some wavelengths. The phase accumulated throughout the crystal changes rapidly with frequency, especially near the band gap.

A unit cell consists of two coax segments, one of 50 ohm RG-58/U and one with 75 ohm RG-59/U. Each segment has the same phase velocity 0.66c and length 8 ft. As a result of impedance mismatch, 20% of the field is reflected at each interface. 12 unit cells of total length 120 m are used. A deep stop gap between 18 and 23 MHz occurs. Outside gap the attenuation is 25 - 35 dB/km. Stop occurs when path length of unit cell is multiple of 1/2.

To calculate dispersive properties and group velocity, the effective index theory is used. The theory says phase shift and scattering loss of the electric field is from an effective complex index of refraction. the real part of the index, nr, is obtained from the overall phase shift f accumulated throught the crystal of length D. t is the complex coefficient of electric field transmission over the whole crystal and m = 0

$$n := 0$$
  $\phi = \arctan\left(\frac{Im(t)}{Re(t)}\right) + n \cdot \pi$   $n_r(\omega) = \frac{c \cdot \phi}{\omega \cdot D}$   $f_{stop} = \frac{v}{2d}$ 

We transmit a sinusoidal carrier with a Gaussian shaped pulse envelope. For carrier of 5 - 15 MHz pulse duration was scaled from 6 to 2 us, keeping the number of cycles within the envelope constant at 30 while varying the bandwidth fro 0.15 to 0.45 MHz.

#### COAXIAL CABLE MODEL

Physical Constant <u>s</u>	Number of Sections, N	$158 := 20 \cdot m$ $159 := 15 \cdot m$
$c := 299792458 \cdot \frac{m}{sec}$	$\mu_0 := 4 \cdot \pi \cdot 10^{-7} \cdot \frac{\text{newton}}{\text{amp}^2}$	$\varepsilon_{0} \coloneqq 8.854187817 \cdot 10^{-12} \cdot \frac{\text{farad}}{\text{m}}$
$\rho_{cu} \coloneqq 1.673 \cdot 10^{-6} \cdot \Omega \cdot cm$	$\sigma \coloneqq \rho_{cu}^{-1} \qquad \qquad \mu_r \coloneqq$	1 $\mu := \mu_0 \cdot \mu_r$ $\lambda o(f) := \frac{c}{f}$

## RG-58/U (50 Ω) and RG-59/U (75 Ω) Coaxial Cable Data:

εr is the dielectric constant Ydb is attenuation in dB

$$\begin{split} \text{Crg58U}_{\text{len}} &\coloneqq 95 \cdot \frac{\text{pf}}{\text{m}} \quad a \coloneqq \frac{1}{2} \cdot 0.9 \text{mm} \quad b \coloneqq \frac{1}{2} \cdot 2.9 \cdot \text{mm} \quad \varepsilon_{r} \coloneqq 2.29 \quad \text{v_cc} \coloneqq 0.66 \quad 158 \coloneqq 8 \cdot \text{ft} \\ \text{Crg59U}_{\text{len}} &\coloneqq 68.6 \cdot \frac{\text{pf}}{\text{m}} \quad a_{59} \coloneqq \frac{1}{2} \cdot 0.81 \text{mm} \quad b_{59} \coloneqq \frac{1}{2} \cdot 3.66 \cdot \text{mm} \quad \text{dB}\_100\text{m} \quad 5,55,500\text{MHz} \quad 0.86,2, \quad 5.7 \\ & v\_c59 \coloneqq 0.66 \quad 159 \coloneqq 8 \cdot \text{ft} \\ \text{Crg62U}_{\text{len}} &\coloneqq \frac{\text{pf}}{\text{m}} \quad a_{59} \coloneqq \frac{1}{2} \cdot 0.81 \text{mm} \quad b_{59} \coloneqq \frac{1}{2} \cdot 3.66 \cdot \text{mm} \quad v\_c62 \coloneqq 0.85 \quad 162 \coloneqq 7.97 \cdot \text{m} \\ & \varepsilon58 \coloneqq \varepsilon_{0} \cdot \varepsilon_{r} \quad d \coloneqq 158 + 159 \\ \text{Ydb}_{\text{Rg58}}(f_{\text{MHz}}) &\coloneqq 1.292 + 1.537 \cdot \sqrt{f_{\text{MHz}}} + 0.0157 \cdot f_{\text{MHz}} \tan \delta \coloneqq 0.0004 \quad f_{\text{gap}} \coloneqq \frac{v\_c\cdot c}{2 \cdot d} \\ & \varepsilon59_{r} \coloneqq \frac{1}{v\_c59^{2}} \quad \varepsilon59 \coloneqq \varepsilon_{0} \cdot \varepsilon59_{r} \end{split}$$



$$Z_{0}(\omega) := \sqrt{\frac{R + j \cdot \omega \cdot L}{G + j \cdot \omega \cdot C}} \qquad Z58_{olc} := \sqrt{\frac{L58_{Len}}{C58_{Len}}} \qquad Z_{0} := 138 \cdot \sqrt{\frac{1}{\varepsilon 59}} \cdot \log\left(\frac{b_{59}}{a_{59}}\right) \qquad Z_{0} = 59.657$$

 $Z58_{olc} = 46.36 \Omega$ 

<u>Attenuation, Phase and Propogation Constants:  $\alpha$ ,  $\beta$ ,  $\gamma$ </u>

$$\begin{split} \gamma(\omega) &= \alpha(\omega) + j \cdot \beta(\omega) \qquad \gamma(\omega) \coloneqq \sqrt{(R + j \cdot \omega \cdot L)(G + j \cdot \omega \cdot C)} \quad \alpha(\omega) \coloneqq \text{Re}(\gamma(\omega)) \qquad \beta(\omega) \coloneqq \text{Im}(\gamma(\omega)) \\ \text{E}(\omega, x) &= \text{E} \cdot e^{-(\alpha(\omega) + j \cdot \beta(\omega)) x} \qquad \text{V}(z) = \text{V}_{\text{incident}} \cdot e^{-\gamma \cdot z} + \text{V}_{\text{reflected}} \cdot e^{\gamma \cdot z} \qquad \alpha_{\text{s}}(f) \coloneqq 2 \cdot \beta(2 \cdot \pi \cdot f) \\ \text{AbsorbCoef}(f) &\coloneqq 10^{-7} \cdot \left(2 \cdot \pi \cdot \frac{\sqrt{f}}{m}\right) \qquad \kappa(f) \coloneqq \sqrt{\mu_0 \cdot \varepsilon_0 \cdot \varepsilon_r} \cdot 2 \cdot \pi \cdot \frac{f}{\sec} + j \cdot \frac{\text{AbsorbCoef}(f)}{2} \text{ wave number} \\ \text{E}(x) &= \text{E}_0 \cdot e^{j \cdot (\kappa \cdot x + \varphi)} \end{split}$$

Material Loss tangent, tanb equals  $jG_{\omega}C$  Thus  $G = j \cdot \omega \cdot C \cdot \tan \delta = 2 \frac{\pi \cdot \varepsilon_{0} \cdot \varepsilon_{1} \cdot \operatorname{length} \cdot \omega \cdot \tan \delta}{\ln\left(\frac{b}{a}\right)}$   $G58(\omega) := j \cdot \omega \cdot \operatorname{Crg58U}_{\text{len}} \cdot \tan \delta$   $G59(\omega) := j \cdot \omega \cdot \operatorname{Crg59U}_{\text{len}} \cdot \tan \delta$  $Z58_{0}(f) := \sqrt{\frac{R58_{\text{Len}}\left(\frac{2 \cdot \pi \cdot f}{\text{sec}}\right) + j \cdot \frac{2 \cdot \pi \cdot f}{\text{sec}} \cdot \operatorname{L58}_{\text{Len}}}{G58\left(\frac{2 \cdot \pi \cdot f}{\text{sec}}\right) + j \cdot \frac{2 \cdot \pi \cdot f}{\text{sec}} \cdot \operatorname{Crg58U}_{\text{len}}}} Z59_{0}(f) := \sqrt{\frac{R59_{\text{Len}}\left(\frac{2 \cdot \pi \cdot f}{\text{sec}}\right) + j \cdot \frac{2 \cdot \pi \cdot f}{\text{sec}} \cdot \operatorname{L59}_{\text{Len}}}{G59\left(\frac{2 \cdot \pi \cdot f}{\text{sec}}\right) + j \cdot \frac{2 \cdot \pi \cdot f}{\text{sec}} \cdot \operatorname{Crg59U}_{\text{len}}}}$ 

#### Reflection and Transmission Coefficients, t and r

From Maxwells Equations: Plane incident E-M wave traveling from medium A to B

$$\begin{split} t_{AB}(f) &\coloneqq \frac{2 \cdot Z59_0(f)}{Z58_0(f) + Z59_0(f)} \\ r_{AB}(f) &\coloneqq \frac{Z59_0(f) - Z58_0(f)}{Z58_0(f) - Z58_0(f)} \\ r_{BA}(f) &\coloneqq \frac{Z58_0(f) - Z59_0(f)}{Z58_0(f) + Z59_0(f)} \\ \end{split}$$

$$M_{BA}(f,j) := \begin{bmatrix} Structure of Lengths of N unit cells starting with Len58 & N := 12 \\ I := 0..N & Len_{58_j} := 158 & Len_{58_0} := 158 & Len_{59_j} := 159 & Len_{59_0} := 0 \cdot m & D := N(d) \\ M_{BA}(f,j) := \begin{pmatrix} -j \cdot \kappa(f) \cdot Len_{58_j} & \frac{j \cdot \kappa(f) \cdot Len_{58_j}}{t_{BA}(f)} & \frac{j \cdot \kappa(f) \cdot Len_{58_j}}{t_{BA}(f)} \\ -j \cdot \kappa(f) \cdot Len_{58_j} & \frac{j \cdot \kappa(f) \cdot Len_{58_j}}{t_{BA}(f)} \end{pmatrix} \\ M_{AB}(f,j) := \begin{pmatrix} -j \cdot \kappa(f) \cdot Len_{59_j} & \frac{j \cdot \kappa(f) \cdot Len_{59_j}}{t_{AB}(f)} & \frac{j \cdot \kappa(f) \cdot Len_{59_j}}{t_{AB}(f)} \\ \frac{e}{t_{AB}(f)} & \frac{j \cdot \kappa(f) \cdot Len_{59_j}}{t_{AB}(f)} & \frac{j \cdot \kappa(f) \cdot Len_{59_j}}{t_{AB}(f)} \\ \frac{e}{t_{AB}(f)} & \frac{j \cdot \kappa(f) \cdot Len_{59_j}}{t_{AB}(f)} & \frac{j \cdot \kappa(f) \cdot Len_{59_j}}{t_{AB}(f)} \\ \end{bmatrix} \end{bmatrix}$$

$$Field Amplitudes, E, for Transmitted and Reflected Waves$$

$$\begin{split} \mathsf{E}(\mathsf{f}) &\coloneqq \left[\prod_{j=1}^{\mathsf{N}} \left(\mathsf{M}_{\mathsf{AB}}\left(\mathsf{f} \cdot 10^{6}, \mathsf{j}\right) \cdot \mathsf{M}_{\mathsf{BA}}\left(\mathsf{f} \cdot 10^{6}, \mathsf{j} - 1\right)\right)\right] \cdot \begin{pmatrix}1\\0\end{pmatrix} \frac{\mathsf{Phase} \ \phi - \mathsf{Effective Index Theory}}{\varphi(\mathsf{f}_{\mathsf{MHz}}) \coloneqq -\operatorname{arg}\left[\left(\mathsf{E}(\mathsf{f}_{\mathsf{MHz}})_{0}\right)^{-1}\right] \\ \mathsf{T}_{\mathsf{s}}(\mathsf{f}_{\mathsf{MHz}}) &\coloneqq \left|\left(\mathsf{E}(\mathsf{f}_{\mathsf{MHz}})_{0}\right)^{-1}\right| \\ \mathsf{T}_{\mathsf{s}}(\mathsf{f}_{\mathsf{MHz}}) &\coloneqq \left|\left(\mathsf{E}(\mathsf{f}_{\mathsf{MHz}})_{0}\right)^{-1}\right| \\ \mathsf{Phz} &\coloneqq \left|\mathsf{G} \leftarrow 0 \\ \mathsf{P}_{\mathsf{1}} \leftarrow \varphi\left(\frac{1}{10}\right) \\ \mathsf{Pold} \leftarrow \mathsf{P}_{\mathsf{1}} \\ \mathsf{for} \ \mathsf{n} \in 2..150 \\ \mathsf{for} \ \mathsf{n} \in 2..150 \\ \mathsf{for} \ \mathsf{n} \in 2..150 \\ \mathsf{g}(\mathsf{f}) &\coloneqq \left(\frac{\mathsf{D}}{\mathsf{c} \cdot \mathsf{T}_{\mathsf{g}}(\mathsf{f})\right) \\ \mathsf{v}_{\mathsf{g}}(\mathsf{f}) &\coloneqq \left(\frac{\mathsf{D}}{\mathsf{c} \cdot \mathsf{T}_{\mathsf{g}}(\mathsf{f})\right) \\ \mathsf{v}_{\mathsf{g}}(\mathsf{f}) &\coloneqq \left(\mathsf{MRE}(\mathsf{PRN}(\mathsf{PhaseBrk}^{\mathsf{r}})) \coloneqq \mathsf{Phz} \\ \mathsf{hereak} &\coloneqq \mathsf{READPRN}(\mathsf{PhaseBrk},\mathsf{prn}^{\mathsf{r}}) \\ \mathsf{P} \end{split}$$

### Calculate Complex Vector Arrays to Store Results for Plotting

$$n := 1 .. 250 \quad \text{freq}_{n} := \frac{n}{10} \qquad \text{E}_{f_{n}} := \text{E}\left(\text{freq}_{n}\right) \qquad \text{T}_{sf_{n}} := \left[\left(\text{E}_{f_{n}}\right)_{0}\right]^{-1}\right] \qquad \varphi_{f_{n}} := -\text{arg}\left[\left(\text{E}_{f_{n}}\right)_{0}\right]^{-1}\right]$$
$$\tau_{gf_{n}} := -\left(\frac{1}{2 \cdot \pi \cdot \frac{10^{6}}{\text{sec}}} \cdot \frac{\varphi_{f_{n}} - \varphi_{f_{n-1}}}{0.1}\right) \qquad \text{v}_{gf_{n}} := \frac{D}{c \cdot \tau_{gf_{n}}} \qquad \text{c}_{vacuum} := 1$$
$$f_{gap} = 2.029 \times 10^{7} \frac{1}{s}$$
$$T_{sf_{0}} := 1 \qquad dbT := \overline{\left(10 \cdot \log\left(T_{sf}\right)\right)}$$







Below are exact solutions. Evaluation was disabled because they take a long time to calculate each function and then repaint each of the graphs

![](_page_4_Figure_2.jpeg)

$$\Delta t := \frac{12 \cdot (158 + 159)}{0.66 \cdot c} \quad \Delta t = 295.768 \text{ nsec}$$
$$n_{r}(f) := \frac{c \cdot \phi(f)}{2\pi \cdot \frac{f}{\text{sec}} \cdot 10^{6} \cdot D} \quad n_{r}(1) = -1.526 \quad f := 1, 1.1..25$$

![](_page_4_Figure_4.jpeg)

mpedance Model

$$\gamma 58(f) \coloneqq \sqrt{\left(R58_{\text{Len}}\left(\frac{2\cdot\pi\cdot f}{\text{sec}}\right) + j\cdot\frac{2\cdot\pi\cdot f}{\text{sec}}\cdot\text{L58}_{\text{Len}}\right)\left(G58\left(\frac{2\cdot\pi\cdot f}{\text{sec}}\right) + j\cdot\frac{2\cdot\pi\cdot f}{\text{sec}}\cdot\text{Crg58U}_{\text{len}}\right)}$$
$$\gamma 59(f) \coloneqq \sqrt{\left(R59_{\text{Len}}\left(\frac{2\cdot\pi\cdot f}{\text{sec}}\right) + j\cdot\frac{2\cdot\pi\cdot f}{\text{sec}}\cdot\text{L59}_{\text{Len}}\right)\left(G59\left(\frac{2\cdot\pi\cdot f}{\text{sec}}\right) + j\cdot\frac{2\cdot\pi\cdot f}{\text{sec}}\cdot\text{Crg59U}_{\text{len}}\right)}$$

$$\begin{split} \text{Z58} \Big( \text{Z}_{\text{L}}, f \Big) &\coloneqq \text{Z58}_{\text{0}}(f) \cdot \left( \frac{\text{Z}_{\text{L}} \cdot \cosh(\gamma 58(f) \cdot 158) + \text{Z58}_{\text{0}}(f) \cdot \sinh(\gamma 58(f) \cdot 158)}{\text{Z58}_{\text{0}}(f) \cdot \cosh(\gamma 58(f) \cdot 158) + \text{Z}_{\text{L}} \cdot \sinh(\gamma 58(f) \cdot 158)} \right) \\ \text{Z59} \Big( \text{Z}_{\text{L}}, f \Big) &\coloneqq \text{Z59}_{\text{0}}(f) \cdot \left( \frac{\text{Z}_{\text{L}} \cdot \cosh(\gamma 59(f) \cdot 159) + \text{Z59}_{\text{0}}(f) \cdot \sinh(\gamma 59(f) \cdot 159)}{\text{Z59}_{\text{0}}(f) \cdot \cosh(\gamma 59(f) \cdot 159) + \text{Z}_{\text{L}} \cdot \sinh(\gamma 59(f) \cdot 159)} \right) \end{split}$$

#### 12 Alternating RG58/59 Sections Cable

 $f_{MHz} := 0, 0.1..25$ 

![](_page_5_Figure_7.jpeg)

VSWR:

The traditional way to determine the reflection coefficient is to measure the standing wave caused by the superposition of the incident wave and the reflected wave. Traditionally the voltage is measured at a series of points using a slotted line. The ratio of the maximum divided by the minimum is the Voltage Standing Wave Ratio (VSWR). The VSWR is infinite for total reflections because the minimum voltage is zero. If no reflection occurs the VSWR is 1.0. VSWR and reflection coefficient are related as follows:

Multiple Reflections If there is a series of impedance changes, each one will cause a reflection. The total reflection is the vector addition of each of the individual coefficients accounting for the distance between discontinuities. Even though the calculations are difficult, a total VSWR can still be measured.

![](_page_6_Figure_0.jpeg)

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